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19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

DAMS, INSPECTION, DAM SAFETY.

Housatonic River Basin Warren, Connecticut

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)
Upper Shepaug Reservoir Dam is a 1,000 foot long earth embankment dam, and has a maximum height of 87 feet. Top width of the dam is 20 feet and appurtenant structures include a side channel spillway, spillway channel and an outlet works. The visual inspection indicated that the dam is in good condition. Based on its intermediate size and high hazard classification the test flood is equal to the PMF.



DEPARTMENT OF THE ARMY

NEW ENGLAND DIVISION. CORPS OF ENGINEERS 424 TRAPELO ROAD WALTHAM. MASSACHUSETTS 02154

REPLY TO ATTENTION OF: NEDED

SEP 2 4 1979

Honorable Ella T. Grasso Governor of the State of Connecticut State Capitol Hartford, Connecticut 06115

Dear Governor Grasso:

I am forwarding to you a copy of the Upper Shepaug Reservoir Dam Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

A copy of this report has been forwarded to the Department of Environmental Protection, the cooperating agency for the State of Connecticut. In addition, a copy of the report has also been furnished the owner, City of Waterbury, 236 Grand Street, Waterbury, Connecticut 06702.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Department of Environmental Protection for your cooperation in carrying out this program.

Sincerely yours,

Incl As stated MAX B. SCHEIDER

Colonel, Corps of Engineers

Division Engineer

UPPER SHEPAUG RESERVOIR DAM CT 00634

HOUSATONIC RIVER BASIN WARREN, CONNECTICUT

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

NATIONAL DAM INSPECTION PROGRAM PHASE I - INSPECTION REPORT BRIEF ASSESSMENT

Identification No.: C

CT 00634

Name of Dam:

Upper Shepaug Reservoir Dam

Town:

Warren

County and State:

Litchfield, Connecticut

Stream:

West Branch of the Shepaug River

Date of Inspection:

December 6, 1978

Upper Shepaug Reservoir Dam is a 1,000 foot long earth embankment dam, and has a maximum height of 87 feet. Top width of the dam is 20 feet and appurtenant structures include a side channel spillway, spillway channel and an outlet works.

Engineering data available consisted of a set of plans dated January, 1963 showing plan, section and details of the dam. No construction specifications or design calculations were available.

The visual inspection of Upper Shepaug Reservoir Dam indicated that the dam is in good condition. The inspection revealed some minor problems including holes up to 3 feet in diameter in the earth berm downstream of the embankment near the left (east) abutment. Riprap indicates sloughing has occurred on the right (west) slope of the outlet channel, small trees were observed in the right (west) wall and floor of the spillway discharge channel. Loose blocks of rock were evident in the spillway channel, standing water was observed on two berms of the downstream slope that is believed to be melt water. A slight bulge up to 1 foot above normal surface was observed on the downstream slope. The dam does not appear to be in jeopardy. Visual inspection also confirmed a well established maintenance program.

Based on its intermediate size and high hazard classification in accordance with the Corps guidelines the test flood is equal to the Probable Maximum Flood. The spillway will pass the test flood outflow of 11,900 cfs with a pool elevation of 920. I feet which is 1.9 feet below the top of the dam.

Based on the findings of the visual inspection and hydrologic and hydraulic analysis, there is no need for further engineering studies or for major alterations to the dam. Provisions should be made by the owner to repair the existing holes in the berm downstream of the embankment

and sloughing riprap on the right (west) side of the spillway discharge channel and remove the trees and loose blocks of rock in the spillway discharge channel.

The recommendations and remedial measures are described in Section 7 and should be addressed within two years after receipt of this Phase I - Inspection Report by the owner.



Robert L. Jones, P.E. Project Manager

Philip W. Genovese & Associates, Inc. Hamden, Connecticut

This Phase I Inspection Report on Upper Shepaug Reservoir Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the Recommended Guidelines for Safety Inspection of Dams, and with good engineering judgment and practice, and is hereby submitted for approval.

OSYPH W. HINEGAN, JR., MEMBER Water Control Branch

Water Control Branch Engineering Division

JOSEPH A. MCELROY, MEMBER

Foundation & Materials Branch

Engineering Division

CARNEY M. TERZIAN, CHAIRMAN

Chief, Structural Section

Design Branch

Engineering Division

APPROVAL RECOMMENDED:

JOE B. FRYAR

Chief, Engineering Division

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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INVENTORY OF DAMS



U.S. ARMY ENGINEER DIV. NEW ENGLAND CORPS OF ENGINEERS WALTHAM, MASS.

PHILIP W. GENOVESE AND ENGINEERS-HAMDEN, CT. ASSOCIATES, INC.

OVERVIEW PHOTO

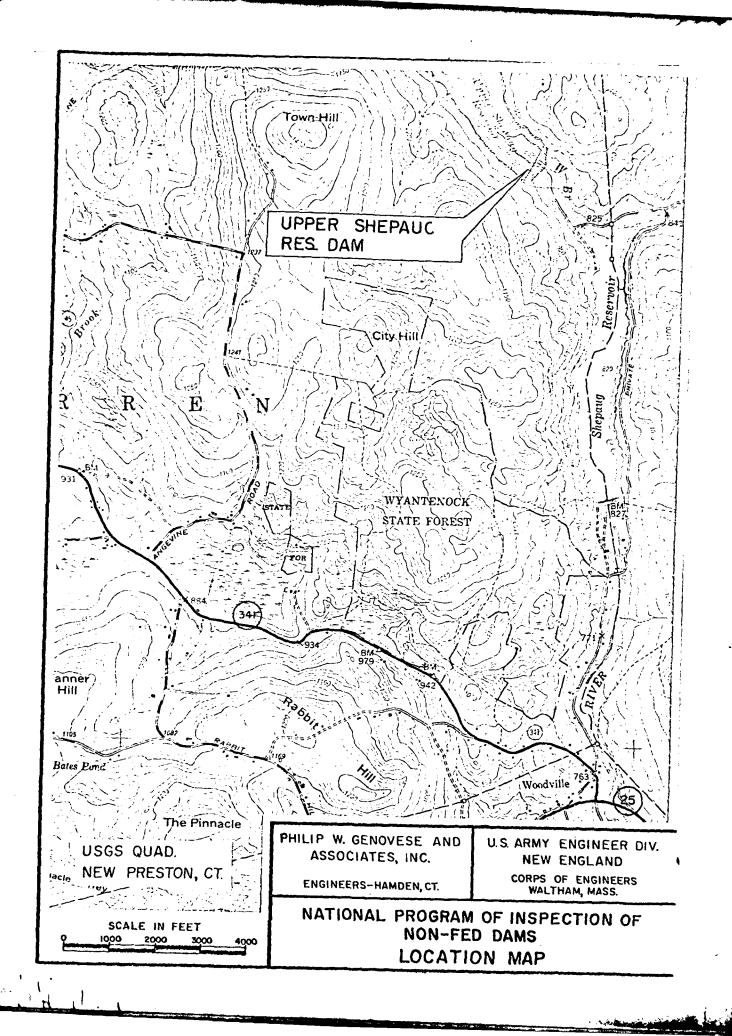
NATIONAL PROGRAM

WEST BRANCH OF SHEPAUG RIVER UPPER SHEPAUG RES DAM

INSPECTION

WARREN, CONN.

NON-FED N F



NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

SECTION 1 PROJECT INFORMATION

1.1 General

a. Authority. Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Philip W. Genovese and Associates, Inc., has been retained by the New England Division to inspect and report on selected dams in the State of Connecticut. Authorization and notice to proceed were issued to Philip W. Genovese and Associates, Inc. under a letter of November 28, 1978 from Max B. Scheider, Colonel, Corps of Engineers. Contract No. DACW 33-79-C0019 has been assigned by the Corps of Engineers for this work.

b. Purpose.

- (1) To perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- (2) To encourage and prepare the states to initiate quickly effective dam safety programs for non-Federal dams.
- (3) To update, verify and complete the National Inventory of Dams.

1.2 Description of Project

a. Location. Upper Shepaug Reservoir Dam is located on the West Branch of the Shepaug River in the Town of Warren, Connecticut, approximately 2.5 miles north of Woodville. The dam is approximately 0.3 of a mile upstream from Shepaug Reservoir which is an impoundment of both the East and West Branch of the Shepaug River. The dam is shown on U.S.G.S. Quadrangle, New Preston, Connecticut with coordinates approximately N41°44.6', W 73°18', Litchfield County, Connecticut. The location of the dam is shown on the Location Map immediately preceding this page.

b. Description of Dam and Appurtenances. Upper Shepaug Reservoir Dam consists of an earth embankment section and a concrete spillway. The embankment section of the dam is approximately 1,000 feet in length. The spillway section has a total length of about 100 feet and is located to the right of the embankment.

Maximum structural height, according to existing plans, is 87 feet for the earth embankment section.

The existing plans indicate that the intake tower of the dam is founded on bedrock.

Appurtenant structures consist of a side channel concrete spill-way, spillway channel and an outlet works structure. The spillway consists of a 100 foot long concrete section at crest elevation of 910 feet. The spillway channel is bounded by concrete retaining walls.

The outlet works consist of a diversion inlet, an intake tower and gate chamber containing 7 gates with two intake pipes and a diversion outlet. Two 30" x 36" sluice gates allow water to enter the intake chamber from two 42" intake pipes at elevation 847.3 feet. Two 48" x 72" sluice gates control flow through the 96" conduit at elevation 833.7 feet to the chamber. The discharge gates to the diversion outlet from the chamber are of elevation 838.0 feet and the drain valve is at elevation 833.5 feet. The sketch in Appendix D shows details of the outlet works.

Figure 1, located in Appendix B, shows the plan of the dam and its appurtenant structures. Photographs of each structure are shown in Appendix C.

- c. Size Classification. Intermediate (hydraulic height-87 feet high, storage 14742 acre-feet) based on storage (> 1,000 to 50,000 acre-feet) as given in Recommended Guidelines for Safety Inspection of Dams.
- d. <u>Hazard Classification</u>. The dam's potential for damage rates it as a high hazard classification. A major breach would result in discharge into Shepaug Reservoir about 1500 feet downstream. Shepaug Reservoir is approximately 6000 feet long. Downstream of the Shepaug Dam about 6000 feet is Woodville which has 12 to 15 houses with 3 low and close to the Shepaug River. There is no habitation downstream of Upper Shepaug Dam to a point downstream of Shepaug Dam.
- e. Ownership. The dam is owned by the City of Waterbury, 236 Grand Street, Waterbury, Connecticut.

- f. Operator. This dam is maintained and operated by the City of Waterbury, Connecticut, Bureau of Water. The superintendent of Reservoirs is Mr. Leonard J. Assard, phone (203) 283-9139.
- g. Purpose of Dam. This dam is used for water supply for the City of Waterbury.
- h. <u>Design and Construction History</u>. Based on State of Connecticut files, the dam was constructed between 1964 and 1965. The "construction permit" is dated December 11, 1964 and the "certificate of approval" is dated December 21, 1965.
- i. Normal Operating Procedure. No data was disclosed for maintenance of reservoir water levels. Under normal operation, two 30 inch x 36 inch sluice gates transmit water from intake pipes to the intake tower. From the gate chamber, two 24 inch fixed cone valves discharge downstream to the diversion outlet. Water then flows down the stream channel to the Shepaug Reservoir.

1.3 Pertinent Data

a. <u>Drainage Area.</u> The drainage area tributary to Upper Shepaug Reservoir consists of approximately 10.4 square miles of mountainous and rolling terrain. In addition to the reservoir, 10 percent of the basin is made up of lake and swamp area. There is no significant development in the drainage area. Elevations in the basin range from about 850 feet to 1,500 feet MSL.

The reservoir consists of about 348 acres at the normal (top of spillway) pool elevation. No dwellings are located along the reservoir shores.

b. Discharge at Dam Site.

- (1) The outlet works for the reservoir consists of two 30 inch by 36 inch intake sluice gates at elevation 847.3 feet and two 48 inch x 72 inch intake sluice gates at elevation 833.7 feet. Water is discharged by two 24 inch fixed cone valves at Q, elevation 838.0 feet. A four inch drain valve is located at elevation 833.5 feet. Water is discharged downstream through an 8 foot diameter diversion outlet pipe. The pipe outlets at elevation 831.5 to a concrete wing wall outlet section. From the outlet section water flows into the stream bed and then to the Shepaug Reservoir approximately 1500 feet downstream.
- (2) There are no records of maximum discharge at the dam site, however, in June, 1977, a depth of flow of 0.75 feet was measured

at the crest of the spillway. This would give a discharge of approximately 300 cfs.

- (3) The spillway capacity with a water surface at the top of dam (elevation 922) would be approximately 18, 200 cfs.
- (4) The spillway capacity with the water surface at the test flood elevation of 920. I feet is approximately 11, 900 cfs.
- (5) The total project discharge at the test flood elevation of 920.1 feet is 11,900 cfs.
 - c. Elevation (feet above MSL).
 - (1) Streambed at centerline of dam 835
 - (2) Maximum tailwater N/A
 - (3) Upstream portal invert diversion tunnel 832.75
 - (4) Recreation pool N/A
 - (5) Full flood control pool N/A
 - (6) Spillway crest (permanent spillway) 910
 - (7) Design surcharge unknown
 - (8) Top dam 922
 - (9) Test flood surcharge 920.1
 - d. Reservoir (miles).
 - (1) Length of maximum pool 2.2
 - (2) Length of recreational pool N/A
 - (3) Length of flood control pool N/A
 - e. Gross Storage (acre-feet).
 - (1) Recreation pool N/A
 - (2) Flood control pool N/A
 - (3) Spillway crest pool 10,090

- (4) Top of dam 14,740
- (5) Test flood pool 13, 942
- f. Reservoir Surface (acres).
 - (1) Recreation pool N/A
 - (2) Flood control pool N/A
 - (3) Spillway crest 348
 - (4) Test flood pool 420
 - (5) Top dam 430
- g. Dam.
 - (1) Type Earthen
 - (2) Length 1,000 feet
 - (3) Height 87 feet (maximum)
 - (4) Top width 20 feet
- (5) Side slopes Upstream: 1:2.75 Downstream 1:2.25 w/berms.
 - (6) Zoning None
 - (7) Impervious core None
 - (8) Cutoff None
- (9) Grout curtain Construction plans indicate the following: weak and shattered rock: to fill seams in rock and any space between rock and masonry work. Grout holes "shall be drilled at the locations ordered."
 - (10) Other Unknown
 - h. Diversion and Regulating Tunnel. See Section j below.
 - i. Spillway.
 - (1) Type Ogee shaped side channel overflow weir.

- (2) Length of weir 100 feet
- (3) Crest elevation 910 feet
- (4) Gates None
- (5) Upstream channel Class "A" concrete and bedrock. Rectangular with Class "A" concrete walls from 5 feet upstream of crest elevation 915 feet.
- (6) Downstream channel Class "A" concrete rectangular channel 20 feet wide from spillway to 161 feet downstream. Walls are vertical and variable in height. From end of concrete section channel is bedrock, 20 feet wide and variable in height with 3 feet minimum.
- j. Regulating Outlets. The reservoir can be drained by a 96 inch outlet pipe set at approximately elevation 838. This pipe is controlled by two 24 inch valves located in the gate chamber building. The four water supply intakes feed the intake tower, gate chamber and diversion outlet. The intakes and outlets are controlled separately by valves located in the intake tower and gate chamber.

SECTION 2 ENGINEERING DATA

2.1 Design

This dam was constructed in 1964 and 1965 for water supply purposes. A set of plans dated 12/58 as prepared by Malcolm Pirnic Engineers showing plan, elevation, typical sections and details is available at the Office of the Engineer, City Hall, Waterbury, Connecticut. No in-depth engineering data were found for this dam.

2.2 Construction

No construction records were avaiable for use in evaluating the dam other than a set of plans marked "As-Built".

2.3 Operation

No engineering operational data were disclosed.

2.4 Evaluation

- a. Availability. Other than the set of plans described above, no additional engineering data was found to be available.
- b. Adequacy. The lack of in-depth engineering data did not allow for a definitive review. Therefore, the adequacy of this dam could not be assessed from the standpoint of reviewing design and construction data, but is based primarily on visual inspection, past performance history and sound engineering judgement.
- c. Validity. The field investigation indicated that the external features of Upper Shepaug Reservoir Dam substantially agree with those on the available plans.

SECTION 3 VISUAL INSPECTION

3.1 Findings

- a. General. The field inspection of the Upper Shepaug Reservoir Dam was made on December 6, 1978. The inspection team consisted of personnel from Philip W. Genovese & Associates, Inc. and Geotechnical Engineers, Inc. Representatives of the City of Waterbury, Bureau of Water were also present during portions of the inspection. Inspection checklists, completed during the visual inspection are included in Appendix A. At the time of the inspection, the water level was approximately 21.5 feet below the permanent spillway elevation. No water was passing over the spillway. The upstream face of the dam could only be inspected above this water level.
- b. Dam. The dam consists of an earthen embankment section about 1000 feet long. The crest is at elevation 922 according to the design drawings.

According to the design drawings, the intake tower gate chamber and spillway are founded on bedrock. The appearance of bedrock outcrops at several locations downstream and adjacent to the spillway is consistent with the design drawings in this respect.

The embankment is covered with grass and appears to be in good condition. The upstream slope is covered with riprap from the toe to an elevation 7 feet above the flow line.

Occasional holes up to 3 feet in diameter occur in an earth berm downstream of the embankment near the left (east) abutment as can be seen in Photos 18, 19 and 20. Informed sources reported the use of rock and boulder fill in the area which suggests that holes are the result of soil collapsing into voids between rock fill. Small bulges and slight depressions on the downstream slope were observed and attributed to differential settlements or minor sloughing. The most pronounced bulge, extending to one foot above the normal slope surface was found approximately 150 feet right (west) of the control tower between the intermediate and lower berm.

Water was observed flowing into the two collection manholes at the downstream toe of the slope.

There is limited information in the available design drawings as to whether the embankment section is founded on bedrock or not. The plans indicate the intake chamber control tower and the spillway are located on bedrock.

No seepage was observed at the downstream slope or downstream toe of the embankment.

c. Appurtenant Structures. Visual inspection of the concrete spillway, spillway channel, and outlet works did not reveal any evidence of stability problems. The concrete surface and construction joints appeared to be in good condition with the exception of occasional cracks and seepage in the spillway discharge channel as seen in Photo 9.

The spillway structure, shown in Photos 6, 7, 9, 10, and 12 consists of an ogee shaped, side channel concrete weir 100 feet long with concrete training walls. The concrete spillway surface is in good condition.

The outlet works consists of a diversion inlet, an intake tower and gate chamber and a diversion outlet that discharges to the stream channel. As the intake structure was below water, it was not inspected. Of the gates located in the gate chamber, four control inlet and two control outlet. Two intakes are at elevation 833.7 feet and two are at 847.3 feet. Two outlets are at elevation 838 feet. All gates are reported to be functional. The discharge conduit is located at elevation 831.5 feet. As all gates were below water in the gate chamber, they could not be inspected. However, all parts of the gate chamber that could be inspected appeared to be in good condition.

The spillway discharge channel is in good condition with the exception of occasional cracks and seeps as shown in Photo 9.

- d. Reservoir Area. The reservoir area has mountainous to rolling terrain, partially wood covered. A more detailed description of the drainage area is included in Section 1.3 of this report. There was no development observed along the shoreline.
- e. Downstream Channel. The spillway discharge channel and the outlet works meet in the stream bed approximately 900 feet downstream of the spillway at approximately elevation 830 feet. The spillway channel is paved for a distance of approximately 270 feet downstream of the spillway as seen in Photo 6. The remainder of the downstream spillway channel is excavated in bedrock as shown in Photo 10. The diversion outlet discharges from the gate chamber through a 96 inch reinforced concrete pipe into a 10 foot wide open channel at elevation 831.5 feet. Minor sloughing of riprap was observed in the right (west) wall of the outlet channel downstream of the diversion outlet.

Occasional loose rocks were observed on the bottom of the spillway discharge channel. A few 2 to 3 inch diameter trees are growing from the right (west) wall of the spillway discharge channel. An 8

inch diameter tree growing from the channel floor was observed near the intersection with the diversion outlet channel as shown in Photo 10. Also minor seepage was observed at joints in the bedrock wall on the right (west) side of the spillway discharge channel.

3.2 Evaluation

Visual examination indicates that the dam is in good condition. No seepage was observed from the foundation or abutments of the embankment sections of the dam. The inspection revealed the following:

- a. Occasional holes in the earth berm adjacent to the embankment.
- b. Small bulges and depressions on the downstream face of the embankment,
- c. Cracks and seepage in the concrete spillway discharge channel.
- d. Minor sloughing of riprap in the outlet channel of the diversion outlet.
- e. Occasional rocks and trees in the spillway discharge channel.

SECTION 4 OPERATIONAL PROCEDURES

4.1 Procedure

Upper Shepaug Reservoir Dam creates an impoundment which is used primarily as a water supply for the City of Waterbury. The normal operational procedure is to draw water from the reservoir and pipe it downstream to the stream bed which flows into Shepaug Reservoir. Water is also discharged through the spillway channel to the Shepaug Reservoir.

4.2 Maintenance of Dam

This dam is visited on a frequent basis by personnel of the City of Waterbury, Bureau of Water. These visits are primarily for surveillance of the reservoir for water quality control purposes. General maintenance is accomplished during these visits.

4.3 Maintenance of Operating Facilities

Maintenance on the operating facilities is done on a regular basis.

4.4 Description of Warning Systems

There are no warning systems in effect at this facility.

4.5 Evaluation

The current operating and maintenance procedures for the dam are to insure that all problems encountered can be remedied within a reasonable period of time. The owner should establish a written operation and maintenance procedure as well as establishing a warning system to follow in event of flood flow conditions or imminent dam failure.

SECTION 5 HYDROLOGY AND HYDRAULIC ANALYSIS

5.1 Evaluation of Features

Upper Shepaug Reservoir Dam is a 1,000 foot long earthen embankment with a 100 foot long concrete spillway. The maximum structural height of the dam is 87 feet. Appurtenant structures other than the spillway consist of a spillway channel and an outlet works. The spillway crest is at elevation 910 feet. The outlet works consist of a diversion inlet, an intake tower and gate chamber and a diversion outlet. The diversion inlet is controlled by two 30 inch x 36 inch and two 48 inch x 72 inch sluice gates and the diversion outlet is controlled by two 24 inch cone valves. The large intake gates are at elevation 833.7 feet and the small gates are at elevation 847.3 feet. Outlets are at elevation 838 feet Q. Upper Shepaug Reservoir Dam is classified as Intermediate in size having a maximum storage of 14,740 acre-feet.

- a. <u>Design Data</u>. No hydrologic or hydraulic design data were disclosed for this dam.
- b. Experience Data. The maximum discharge at this dam site is unknown. The maximum observed condition was reported to be nine inches over the spillway or about 300 cfs.
- c. <u>Visual Observations</u>. No evidence of damage to any portion of the project from overtopping was visible at the time of the inspection.
- d. Test Flood Analysis. As no detailed design and operational information are available, hydrologic evaluation was performed using dam information gathered by field inspection, watershed size and an estimated test flood equal to the Probable Maximum Flood (PMF) as determined by guide curves issued by the Corps of Engineers. Based on a drainage area of 10.4 square miles, it was estimated that the test flood flow at this dam would be 18,720 cfs. Following the guidance for Estimating Effect of Surcharge Storage on Maximum Probable Discharges results in a test flood discharge of 11,900 cfs. As the maximum spillway capacity at the top of the dam is 18,212 cfs, the spillway will pass the PMF without over topping the dam.
- e. <u>Dam Failure Analysis</u>. The impact of failure of the dam at maximum pool (top of dam) was not assessed using the "Rule of Thumb" Guidance for Estimating Downstream Dam Failure Hydrographs issued by the Corps of Engineers.

A downstream routing was not accomplished as there is only about 1,500 feet of uninhabited valley that lies between Upper Shepaug Dam and the upstream reaches of Shepaug Reservoir, both important water supply facilities for the Waterbury area. Shepaug Dam was breached and downstream water profile to Woodville was established.

Relative storage capabilities of Upper Shepaug and Shepaug Reservoir Dams are:

	Upper Shepaug	Shepaug
Storage to Spillway Crest (Ac-Ft.)	N/A	2,000
Storage to top of dam (Ac-Ft.)	14,700	3,000

An analysis using a breaching outflow of 237, 600 cfs and utilizing the discharge rating curve and data for Shepaug Reservoir Dam, the surcharge would be 33.5 feet above the spillway crest of Shepaug Dam.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

- a. <u>Visual Observations</u>. The visual examination did not disclose any immediate stability problems. Routine maintenance should be sufficient to prevent any long-term problems.
- b. <u>Design and Construction Data</u>. Design drawings are available for the dam. They include general information regarding the overall dimensions of the dam and appurentenances. This information is not sufficient to assess the stability of the dam and it must be judged primarily from visual observations. Grouting of the bedrock was required by the contract documents but the details are not available.
- c. Operating Records. No operating records pertinent to the structural stability of the dam were available.
- d. <u>Post Construction Changes</u>. Since original construction in 1964 and 1965 no significant changes or additions have been made at the site.
- e. <u>Seismic Stability</u>. The dam is located in Seismic Zone I, and in accordance with recommended Phase I guidelines does not warrant seismic analysis.

SECTION 7 ASSESSMENT, RECOMMENDATIONS AND REMEDIAL MEASURES

7.1 Dam Assessment

- a. <u>Condition.</u> The visual examination indicates that the dam is in good condition. The inspection revealed:
- (1) Occasional holes up to 3 feet in diameter in the earth berm adjacent to the downstream side of the embankment near the left (east) abutment.
- (2) Small bulges and slight depressions on the downstream face of the embankment. The most pronounced bulge about 1 foot above the normal slope was found about 150' right (west) of the control tower.
- (3) Cracks and seepage in the concrete spillway discharge channel.
- (4) Minor sloughing of riprap in the right (west) wall of the outlet channel downstream of the diversion outlet.
- (5) Occasional rocks and trees in the bedrock portion of the spillway discharge channel.
- b. Adequacy of Information. The lack of in-depth engineering data did not allow for a definitive review. Therefore, the adequacy of this dam could not be assessed from the standpoint of reviewing design and construction data, but is based primarily on visual inspection, past performance history and sound engineering judgement.
- c. <u>Urgency</u>. This dam is in good condition and no recommendations are required. The remedial measures described in Section 7.3 should be accomplished within two years after receipt of this Phase I Inspection Report by the owner.
- d. Need for Additional Investigation. The findings of this inspection indicate that there is no need for additional investigations.

7.2 Recommendations

Based on the findings of the visual inspection and hydrologic and hydraulic analysis there is no need for further engineering studies or for major alterations to the dam.

7.3 Remedial Measures

- (a) Existing holes in the downstream berm near the left (east) abutment should be backfilled and appropriate cover planted. If and when new holes appear, they should be routinely examined and backfilled.
- (b) Sloughing riprap on the right (west) slope of the outlet channel should be repaired.
- (c) Small trees in the right (west) wall and the 8 inch diameter tree in the floor of the spillway discharge channel should be removed. Also, all loose blocks of rock in the channel floor should be removed.
- (d) Establish an operational procedure and formal warning system to follow for emergency conditions.
 - (e) Develope a biennial technical inspection program.

7.4 Alternatives

There is no practical alternative to the recommendations in Sections 7.2 and 7.3.

APPENDIX A

INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST PARTY ORGANIZATION

PROJECT: UPPER (Carri		DATE: December 6.	. 1978	
Crest of dam	922.0	TIME: 1300 WEATHER: Sunny- 40°-50°		
Spillway Cres	st 910.0	W.S. ELEV. 888 55	-	
PARTY:		W. 15. E 1513 V. LINING. 1.2	. U . Ma	
1. Bob Jones	Party Chief			
2. Don Ballou	Hydraulics/Hydrology			
3. Karl Dalenber	Geotechnical			
4. Dick Murdock	11			
5. Leonard Assard	Owner's Rep.			
PROJEC	CT FEATURE	INSPECTED BY	REMARKS	
1.				
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8				
				
		Martin Martin Martin and Artin Annie (1904), and a state of the state		
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PERIODIC INSPECTION CHECKLIST PROJECT: UPPER SHEPAUG DAM DATE: December 6, 1978 PROJECT FEATURE: Earthen Dam Embankment NAME DISCIPLINE NAME

	AREA EVALUATED	CONDITION
	DAM EMBANKMENT	
ıΒ	Crest Elevation	922.0' USGS
ŊΒ	Current Pool Elevation	888.55' USGS
ВЈ	Maximum Impoundment to Date	910.75' <u>+</u> USGS
EI	Surface Cracks	None
~EI	Pavement Condition	Gravel roadway
GEI	Movement or Settlement of Crest	None observed
EI	Lateral Movement	None observed
ΕI	Vertical Alignment	Good
GEI	Horizontal Alignment	Good
_EI	Condition at Abutment and at Concrete Structures	Slight surface erosion at gatehouse
ωEI	Indications of Movement of Structural Items on Slopes	None
∟EI	Trespassing on Slopes	None
EI ما	Sloughing or Erosion of Slopes or Abutments	Minor surface slough 3751 left (east) of spillway on downstream slope near 2nd berm
GEI	Rock Slope Protection-Riprap Failures	Good, random blocks, no failures
EI	Unusual Movement or Cracking at or Near Toe	None
EI	Unusual Embankment or Downstream Seepage	None
EI	Piping or Boils A-2	None

	PERIODIC INSPECTION CHECKLIST				
	PROJECT: UPPERSHEPAUG DAM	DATE: December 6, 1978			
	PROJECT FEATURE: Earthen Dam Emb	pankment NAME			
	DISCIPLINE	NAME			
	AREA EVALUATED	CONDITION			
	DAM EMBANKMENT - Continued				
GEI	Foundation Drainage Features	Slight flow out of toe drains into manholes at downstream toe.			
GEI	Toe Drains	Water elevation in right manhole is 4'9" below top of manhole & in left manhole 10'6" below top			
GEI	Instrumentation System	None			
GEI	Vegetation	Well maintained grass slopes			
		, i			
	A-3	,			

PERIODIC INSE	PECTION CHECKLIST
PROJECT UPPER SHEPAUG DAM	DATE: December 6, 1978
PROJECT FEATURE Other Embankment	NAME
DISCIPLINE	NAME
AREA EVALUATED	CONDITION
DIKE EMBANKMENT	
Crest Elevation	None
Current Pool Elevation	
Maximum Impoundment to Date	
Surface Cracks	
Pavement Condition	
Movement or Settlement of Crest	
Lateral Movement	
Vertical Alignment	
Horizontal Alignment	
Condition at Abutment and at Concrete Structures	
Indications of Movement of Structural Items on Slopes	
Trespassing on Slopes	
Sloughing or Erosion of Slopes or Abutments	
Rock Slope Protection-Riprap Failures	
Unusual Movement or Cracking at or Near Toes	
Unusual Embankment or Downstream Seepage	
Piping or Boils	
Foundation Drainage Features	
Toe Drains	
Instrumentation System	
Vegetation	

A-4

	PERIODIC INSPECT	ION CHECKLIST	
PRC	JECT UPPER SHEPAUG DAM	DATE: December 6, 1978	
PRC	JECT FEATURE: Outlet Works-Intal	e NAME	
DISC	IPLINE	NAME	
		·	
	AREA EVALUATED	CONDITION	
OUT	LET WORKS - INTAKE CHANNEL AN INTAKE STRUCTURE	<u>b</u>	
a.	Approach Channel	Under water, not observed	
	Slope Conditions		
	Bottom Conditions		
	Rock Slides or Falls		
	Log Boom		
	Debris		
	Condition of Concrete Lining		
	Drains or Weep Holes		
b.	Intake Structure		
	Condition of Concrete		
	Stop Logs and Slots		
	A-5		

PERIODIC INSPECTION CHECKLIST

PROJECT: UPPER SI	HEPAUG DAM	DATE December 6, 1978
PROJECT FEATURE	Outlet Works - Tower	NAME
DISCIPLINE		NAME

		AREA EVALUATED	CONDITION
		TLET WORKS - CONTROL TOWER	
	a.	Concrete and Structural	
J		General Condition	Good
ВЈ		Condition of Joints	Good
۳J		Spalling	None
J		Visible Reinforcing	None
ВЈ		Rusting or Staining of Concrete	None
~J		Any Seepage or Efflorescence	None
,J		Joint Alignment	Good
ВЈ		Unusual Seepage or Leaks in Gate Chamber	None
вJ		Cracks	None
J		Rusting or Corrosion of Steel	None
	ь.	Mechanical and Electrical	
		Air Vents	Gates and operating mechanisms are located in control tower.
		Float Wells	Control mechanisms are in good condition.
		Crane Hoist	Gates not accessible for inspection.
		Elevator	
		Hydraulic System	
		Service Gates	
	[Emergency Gates	
		Lighting Protection System	
		Emergency Power System	
		Wiring and Lighting System	

A-6

PERIODIC INSPEC	TION CHECKLIST
PROJECT: UPPER SHEPAUG DAM	DATE December 6, 1978
PROJECT FEATURE Outlet Works	NAME
DISCIPLINE	NAME———
AREA EVALUATED	CONDITION
OUTLET WORKS - TRANSITION AND CONDUIT	N/A
General Condition of Concrete	
Rust of Staining on Concrete	
Spalling	
Erosion or Cavitation	
Cracking	
Alignment of Monoliths	
Alignment of Joints	
Numbering of Monoliths	
A-7	

PERIODIC INSPECTION CHECKLIST PROJECT: UPPER SHEPAUG DAM DATE December 6, 1978 PROJECT FEATURE Outlet Works - Channel NAME

DISCIPLINE NAME

	AREA EVALUATED	CONDITION
	OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL	
зJ	General Condition of Concrete	Fair
ЗJ	Rust or Staining	Some
ВЈ	Spalling	Some
	Erosion or Cavitation	
ij	Visible Reinforcing	Some
ВЈ	Any Seepage or Efflorescence	Some seepage through cracks
ىJ	Condition at Joints	Fair to poor
EI	Drain holes	None
GEI	Channel	Sloped riprap sides, good condition
GEI	Loose Rock or Trees Overhanging Channel	None
GEI	Condition of Discharge Channel	Good
	A-8	

PERIODIC INSPECTION CHECKLIST PROJECT: UPPER SHEPAUG DAM DATE December 6, 1978 PROJECT FEATURE Outlet Works - Spillway NAME DISCIPLINE-- NAME AREA EVALUATED CONDITION OUTLET WORKS - SPILLWAY WEIR. APPROACH AND DISCHARGE CHANNELS Approach Channel General Condition Good Loose Rock Overhanging Channel None Trees Overhanging Channel None Floor of Approach Channel Sand & gravel floor, good condition Weir and Training Walls b. General Condition of Concrete Good Rust or Staining Some Spalling None Any Visible Reinforcing None Any Seepage or Efflorescence On abutment side slight seepage through joints and cracks of concrete wall. Drain Holes Many on abutment side, some seeping ic. Discharge Channel General Condition Good Loose Rock Overhanging Channel None observed Trees Overhanging Channel None observed Floor of Channel Concrete floor adjacent to embankment in bedrock surface ending in loose rock at downstream end. Other Obstructions One 6"-8" tree in center of spillway

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A-9

at downstream end.

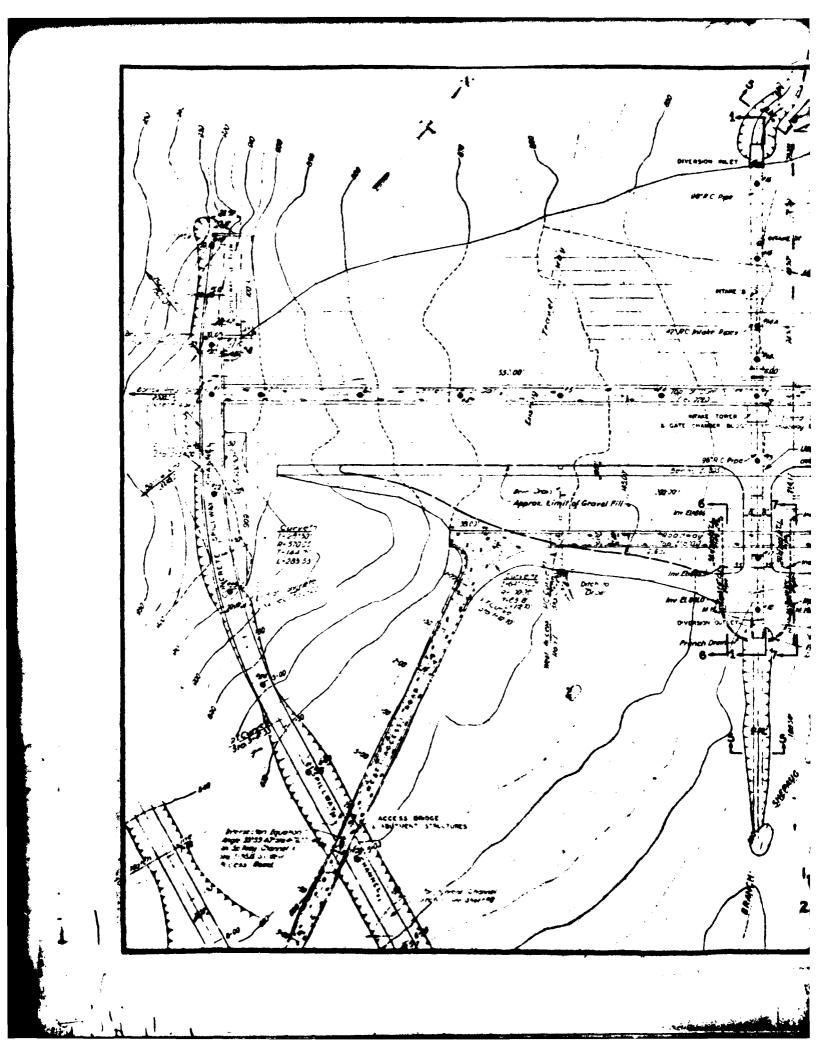
	DEDIONIC INCOM	CONTONI CLIE	COLLI ICID	
PERIODIC INSPECTION CHI PROJECT: UPPER SHEPAUG				
	PROJECT FEATURE Outlet Works DISCIPLINE		NAME	
DIS				
	AREA EVALUATED		CONDITION	
OUT	LET WORKS - SERVICE BRIDGE			
a.	Super Structure	None		
	Bearings			
	Anchor Bolts			
	Bridge Seat			
	Longitudinal Members			
	Underside of Deck			
	Secondary Bracing			
	Deck			
	Drainage System			
	Railings			
	Expansion Joints			
	Paint			
ь.	Abutment & Piers			
	General Condition of Concrete			
	Alignment of Abutment			

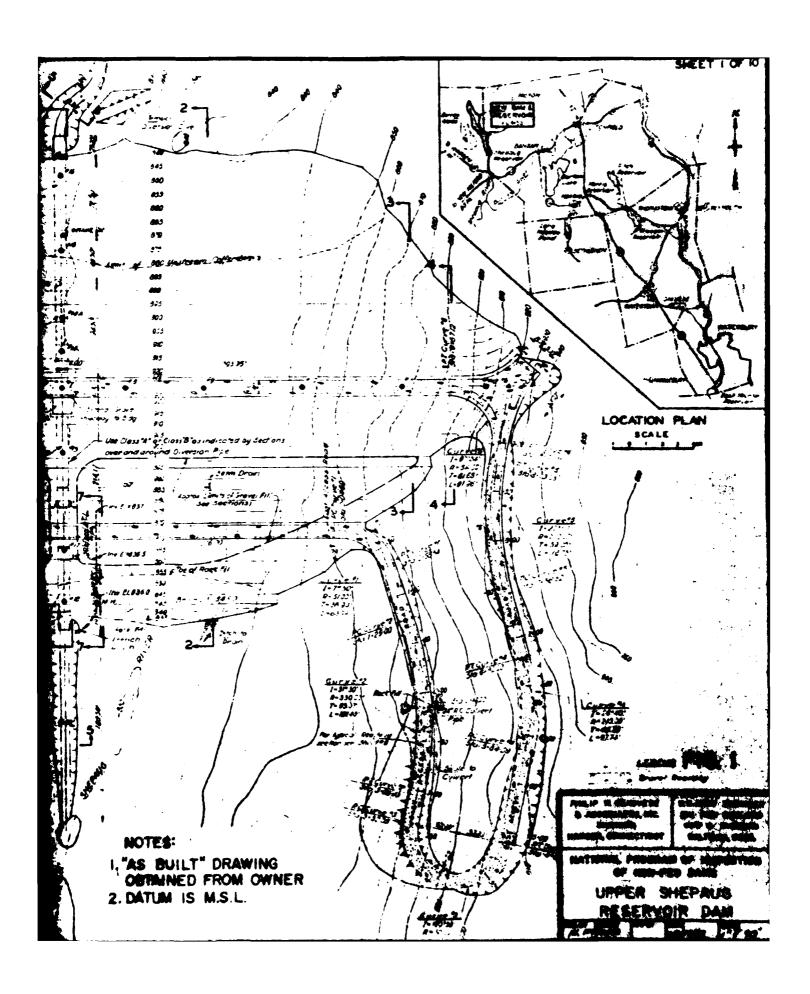
Approach to Bridge

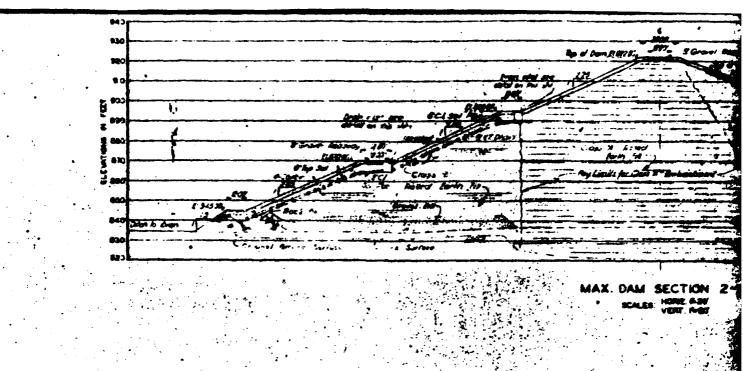
Condition of Seat and Backwall

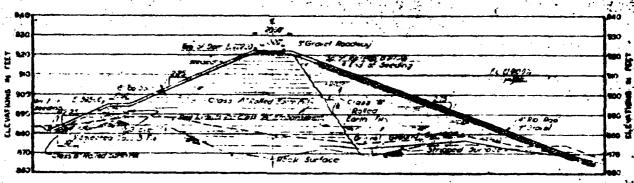
APPENDIX B

ENGINEERING DATA

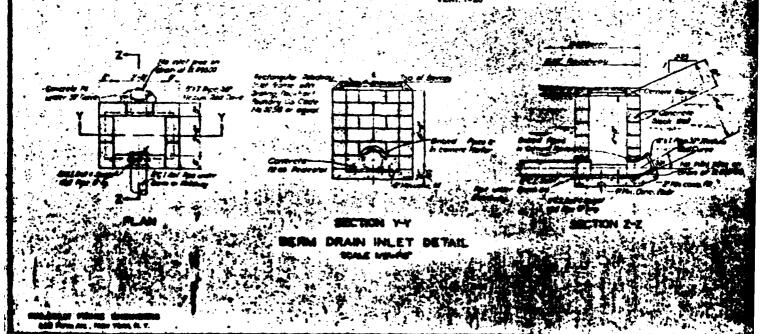


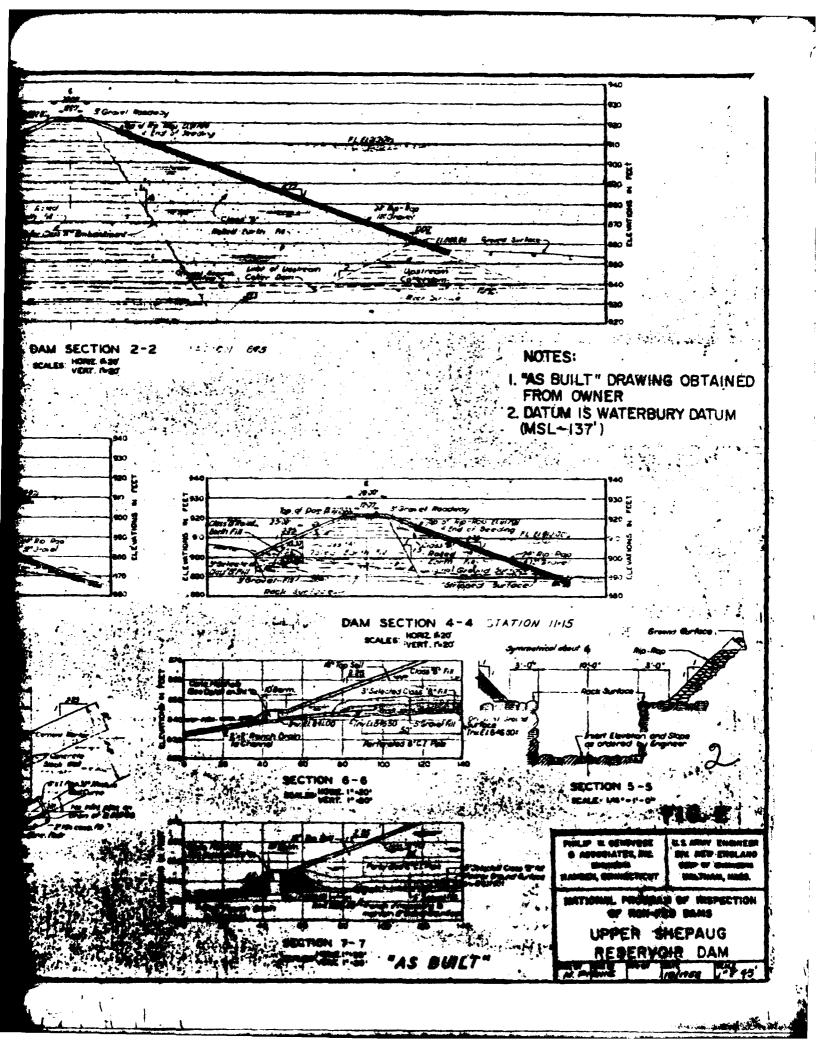






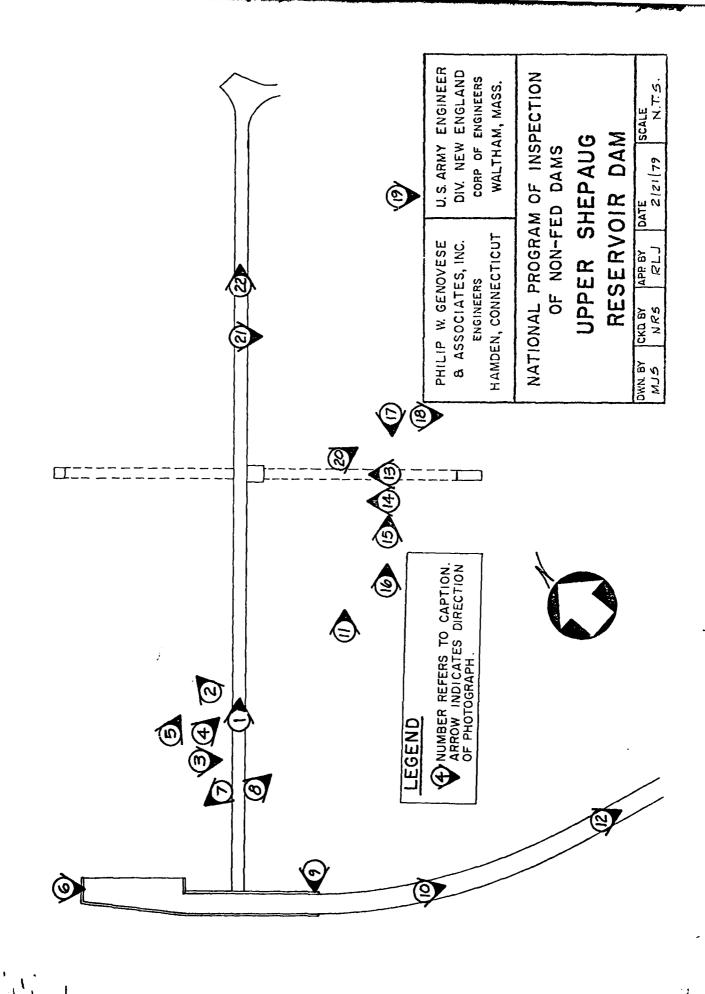
DAM SECTION 3+3 STATION 10-75





APPENDIX C

PHOTOGRAPHS



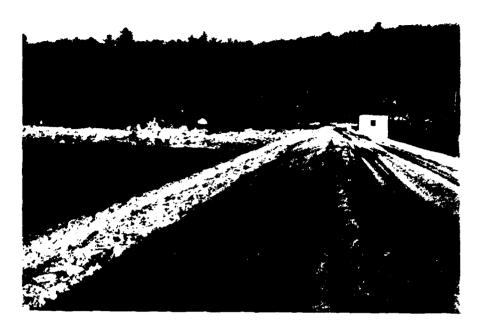
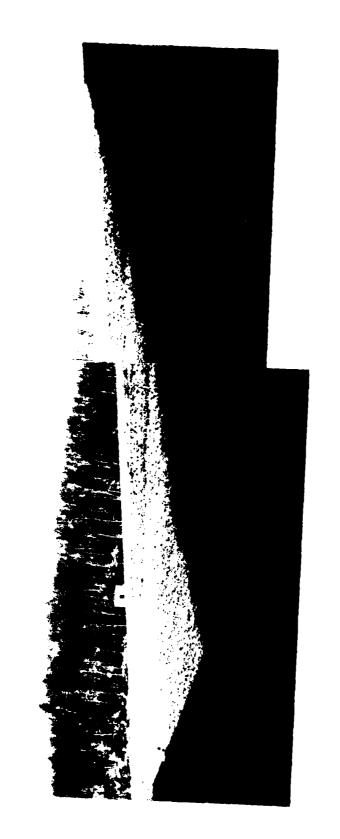


PHOTO NO. 1 - Looking along upstream face toward east abutment, 150' left (east) of spillway channel.



PHOTO NO. 2 - Looking upstream at riprap, 150' left (east) of spillway channel.



PHOTOS NO. 3, 4 and 5 - Panorama of three shots from right (west) side toward left (east) abutment. Showing upstream face of dam, Note upstream spillway training wall in extreme right.





PHOTO NO. 6 Spillway channel looking downstream from right (north) training wall of side channel spillway.



PHOTO NO. 7 - Looking toward side channel spillway approach channel from 100 feet left (east) of spillway channel.

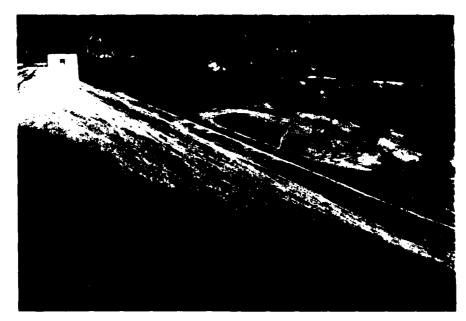


PHOTO NO. 8 - Looking along downstream face toward left (east) abutment from crest 100' left (east) of spillway channel.

PHOTO NO. 9 Crack in spillway training wall, right (west) side, approximately 100' downstream from crest.



PHOTO NO. 10 Looking downstream along spillway channel from end of training wall.



PHOTO NO. 11 View along second berm, standing water, slight flow may be surface runoff, rule extended three feet.



PHOTO NO. 12 Looking downstream along outlet channel.



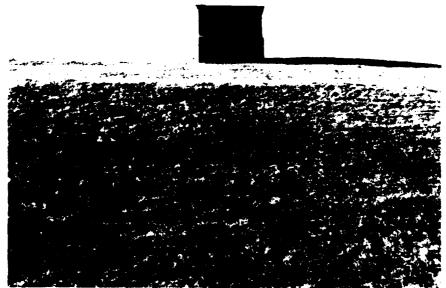


PHOTO NO. 13 - Looking upstream at downstream slope from right (west) edge of outlet training wall.

PHOTO NO. 14 Looking upstream along 4" diameter underground drain outlet from 2" diameter drainage manhole.



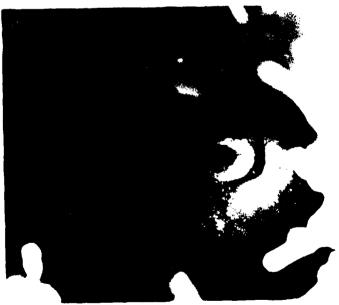


PHOTO NO. 15 - 6" diameter discharge pipe in drainage manhole, depth of water 4'9" below manhole cover, right (west) manhole.

PHOTO NO. 16 Drainage manhole at downstream toe looking toward left (east) abutment.





PHOTO NO. 17 - 6" diameter discharge pipe in east drainage manhole, water depth 10" 6".



PHOTO NO. 18 - Hole downstream of toe, due to settling of soil around large boulder placed during construction of dam. Rule extended 3 feet, location 50' east of diversion outlet.



PHOTO NO. 19 Large holes, up to 2 feet deep, downstream of dam 200 feet left (east) of diversion outlet. Rule extended 3 feet.



PHOTO NO. 20 - Looking downstream at toe from diversion outlet. Holes in center are those shown in Photo No. 18.



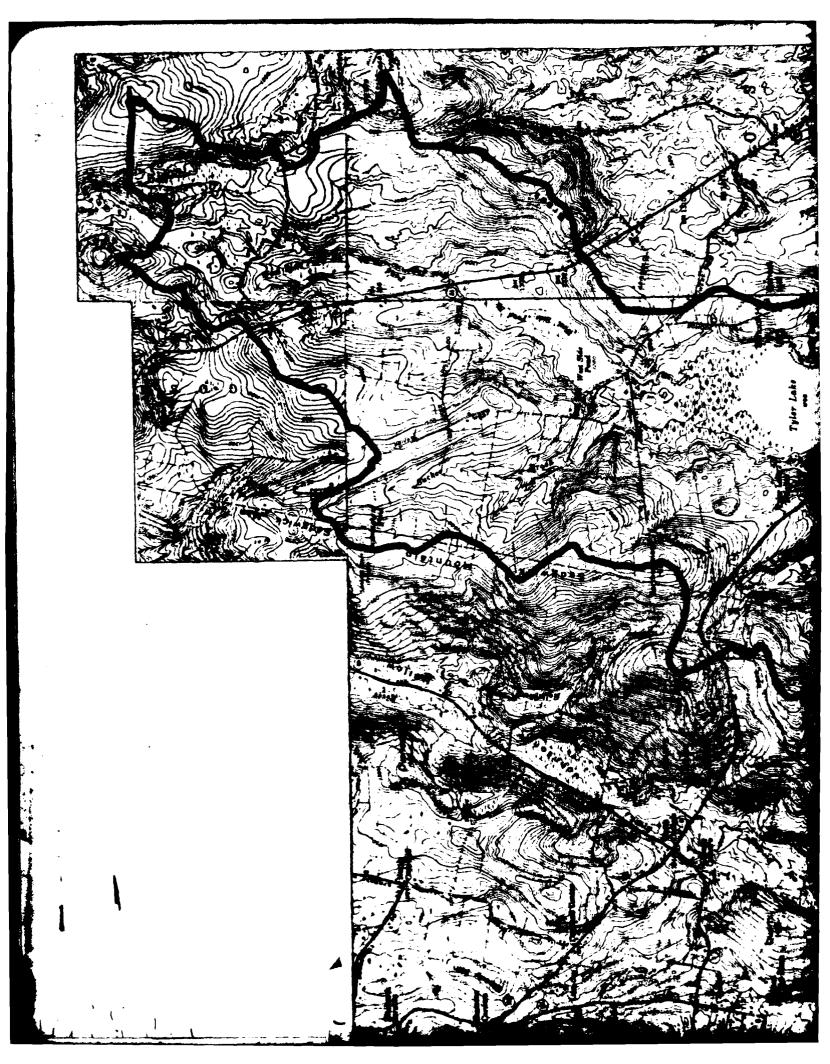
PHOTO NO. 21 - Looking along downstream slope from crest of dam 50 feet left (east) of tower.

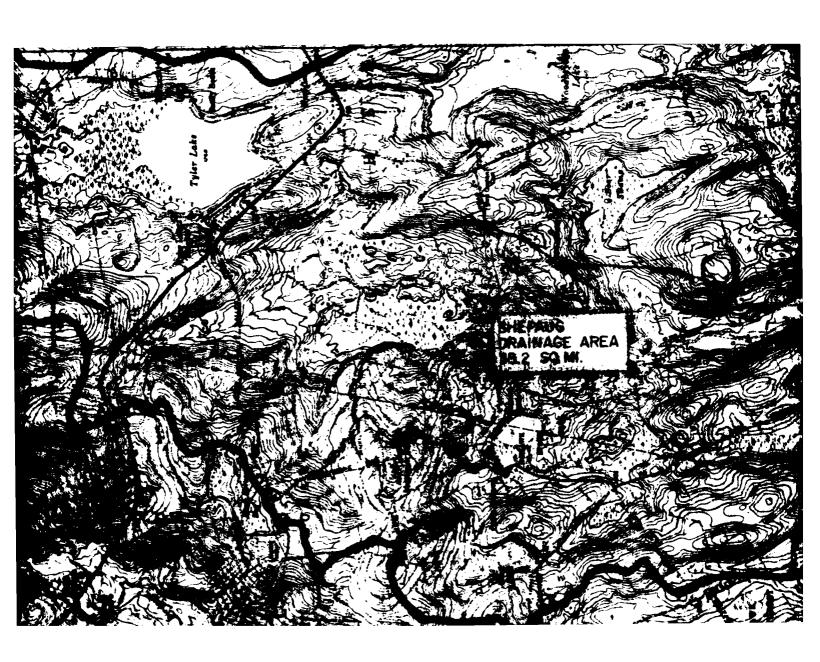


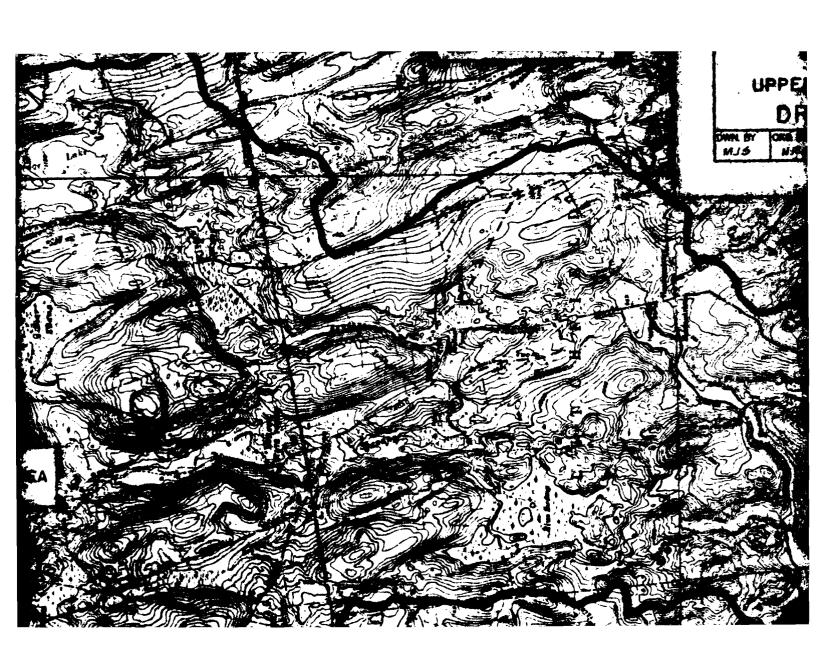
PHOTO NO. 22 - Looking toward left (east) abutment from upstream crest 75 feet left (east) of tower.

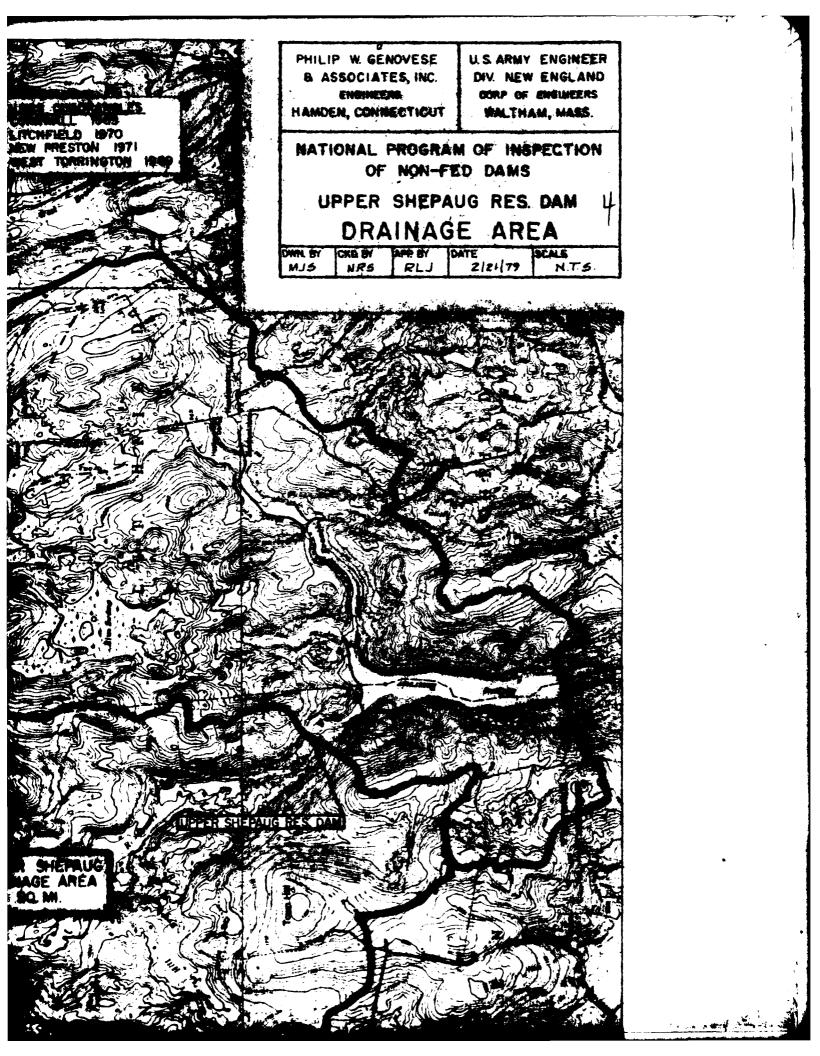
APPENDIX D

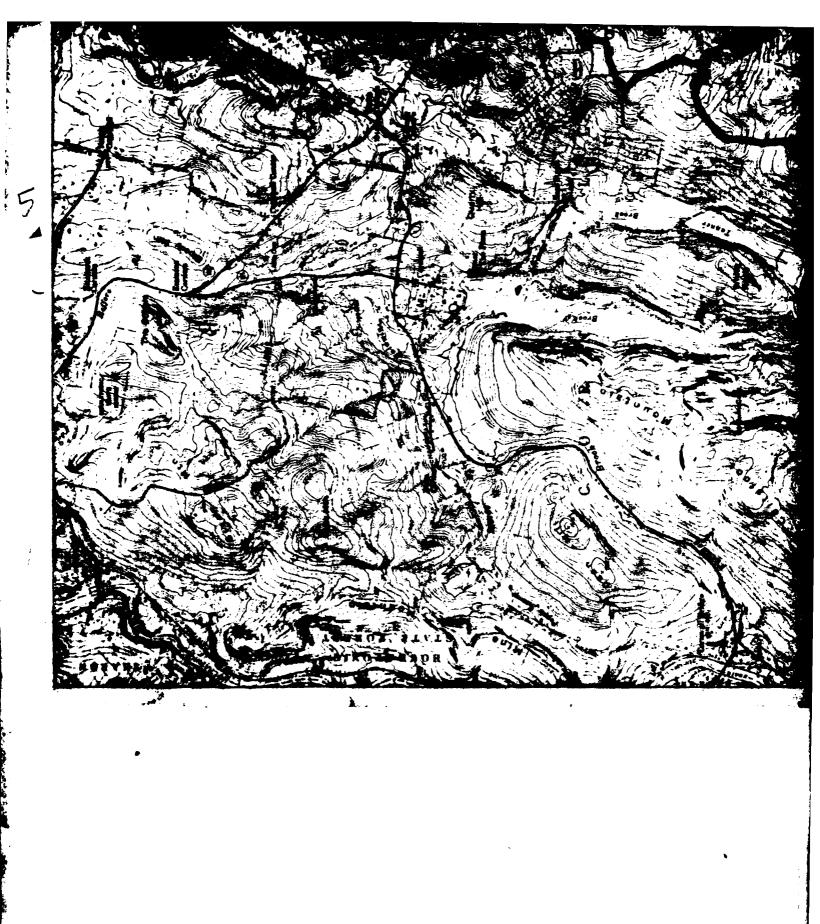
HYDROLOGIC AND HYDRAULIC COMPUTATIONS





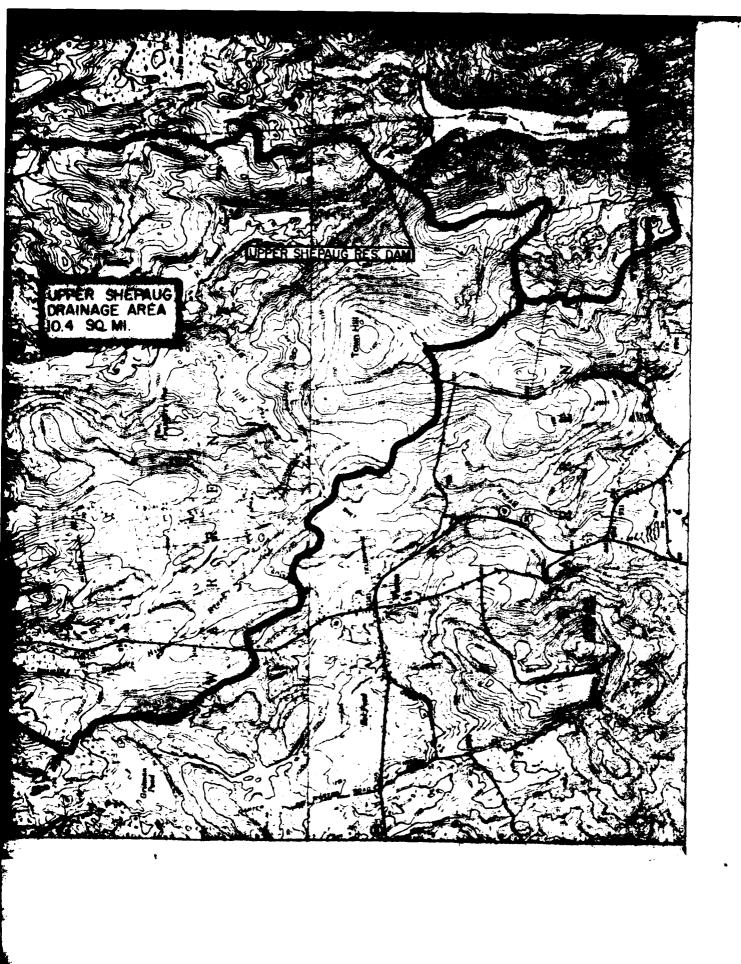






Access to the second





	Page Feb 1979
Name -	
Location	- Warren, Ct.
Drainage Area	6656 Acres/10.4 sq-miles
Spillway Crest	Elev 910.0
Top of Dam	- Elev 922.0
Dam Height	
Size E, Hazard	-Intermediate - High
Test Flood (TF)	PMF
TF Runoff	- 19"
TF Peak Discharge	18,720 c Pz
TF Volume	10,538 AC-Ft
spillway storage	- 4,650 Ac-Ft (NO Freeboard)
Opeak Outflow	-11,900 cfs
Stage @ Apar Outflow	Ekv 920.1
Storage @ Perk Outflow -	-3880 Ac-Ft
spillway Type	Concrete Oger Shaped with Side Channel Spillway
Breaching Discharge -	-237,572 CFS

Evaluate the Size" of Itajare" classification of the dam in order to arrive a the magnitude of the spillway design storm (SDF) (text sterm)

Use tables # 1,25,3 of the DOA. OCE.
guidelines dated Nov. 1976

Size classification

- (a) Top of Dam plov = 922.0

 downstram lowpoint elev = 835.0

 Height of Dam = 87.0 feat
- (b) Reservoir area @ Flow line = 348 acres (elar 9100)

 = Estimated volume below blow line
 = 1/3 bh = \frac{1}{3} x 348 x 87' = 10,092 Ac-Ft.

Notione between Flowline c' top of Dam
15 4650 AC-Ft for a total maximum
Storage corpacity of 14,742 AC-Ft

Hence, from table #1 the size classification is Intermediate

Hazard Petential

while there appears to be no Nabitation of any form immediately downstream of the dam it should be noted that Shepauq Dam Reservain is immediately downstream by about 1500 feet. The reservain itself being a water supply for the City of Waterbury and

Feb 1979 By D.T.E.H

approximately 6000 feet in length. Downstream of Shepang Dam by 6000 feet is

the town of Woodville. The valley that

lies between woodville e' Shepang Dam has
approximately 12 - 15 houses with three
houses quite low e' close to the Shepang
River. Because of those relationships
it is felt that a hagard classification
of High Should be placed on

upper Shepang Dam

Spillway Darian Storm (SDF) (Test Storm)

From table H3 of the O.C.E. quidos entoring with a zize classification of intermediate and a hazard hotential of High a SDF of PMF 12 recommended.

The conformations were done for both
the PMF & KPMF, however. the PMF
15 5111 The selected Test Flood (SDF)

Nsing data founished by the Corp NED; a drainage area of 10.41 sq-miles, and a D.A. terrain that would appear to fell somewhere between "Rolling" & Mountainous the SDF are as follows:

rolling = 1640 csm Mountaines = 1970 csm

Feb 1979 By: D.T. Balbu

Select a CSM value of 1800 which is about half-way between ralling & Mountainous of PMF = 1800 CPS/mi x10.4 mi = 18720 CPS

and 1/2 PMF = 9360 C95

Find Runoff volume in 12 PMF E. PMF

Note:

THE PMF has 19" of R.O.

D.A. = 10,4 sq-m, Hes

VpmF = (53.33 Ac-Ft/in Rd./mi.)(10.4)(19) = 10,538 Ac-Ft

V/2 PMF = 5,269 AC-Ft

Note that there is 4,650 Ac-Ft of available sterage between the spillway exet & the top of dam (Stegraph next page)

Check hydrograph time of PMF:

1 x 5.45 x 2 = T

= 10,538 x 2 4.2 x 18720 = 13.6 hours

Note: 1/2 PMF would have same time.

D 100 200 200 400 SURFACE AREA -ACRES	500 Page 5
925	
724	
423	
-922 iii	
921-1	
920	
919 (A)	
10 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
916	
915 Top 6	
	Upper Shopang Dam
	Fe'5, 1979
912 211	13 0 1 Eq. 194
5CHO	
2000 3000 4000	5000 6000
	CREST -AC-FT

To June 1

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Work up Rating Corve for Service : spillway

The spillway is 100' long, oyer shaped, and training walls that extend to a Neight of 5' above the spury crest; evaluate this section and the overflow that occurs above this point. (See sketch Below)

Oburthousedon = CLH W whore C= 3.9 E' L = 100'

Elev	Head	H 3/2	\mathbb{Q}	Hoverflow	anallar Bo	Qroral
MSL	ţt		ctr	Tretien	cf t grethu	cfs
910	0	O	0			0
911	1	1	390			390
912	2	2.83	1103			1103
913	3	5-20	2026	_		2505
914	મ	8	3120			3120
915	5	11.18	4360			4360
916	6	14.70	5732	t	$\mathcal{B}o1$	5840
917	7	18.52	7223	Z	306	7529
918	8	22.63	8825	3	562	9387
919	9	27	10,530	4	864	11,394
920	10	31.62	12,333	5	1207	13,540
922	12	41.57	16,212	7	2000	215,81

922 12 41.57 16,212 7 2000

El 522.0 (Top of Dam)

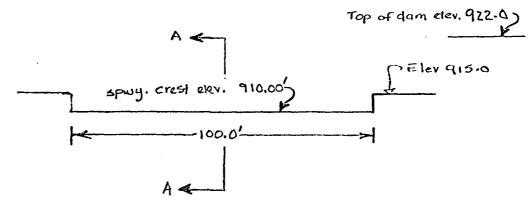
Service Spillway

Section Looking Downstream

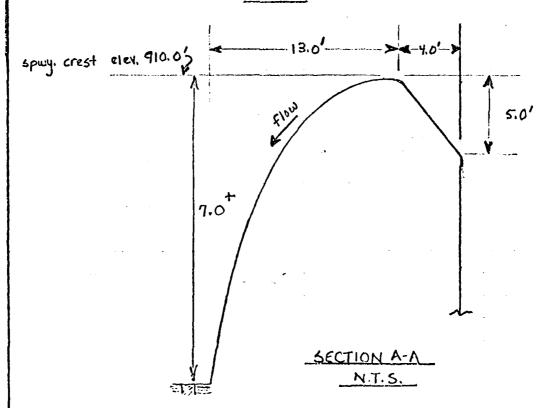
Jan.1979

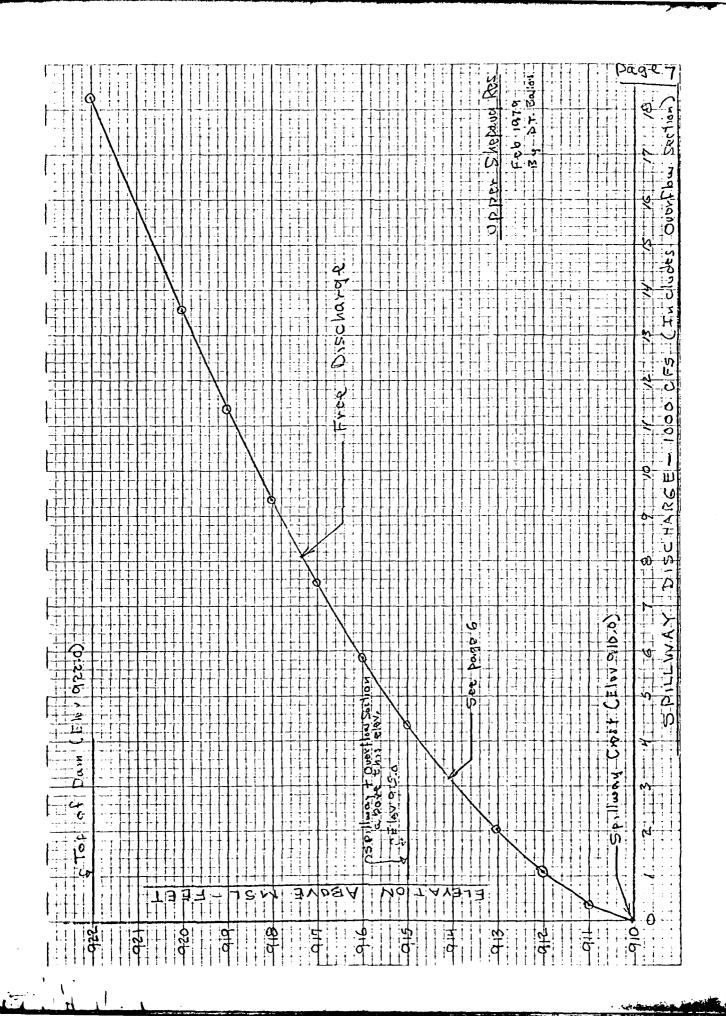
UPPER ShePAUGRESERVOIR, Warren, Conn.

SERVICE SPILLMAY



ELEVATION VIEW
LOOKING UPSTREAM
N.T.S.

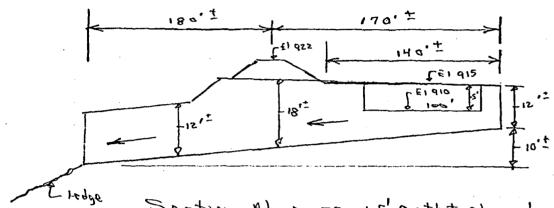




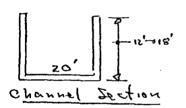
Side Channel Discharge

Feb 1979 By: b.T. Ballow

Evaluate existing concrete channel that is the outlet channel downstream of the service spillway-(This may be a control)



Section Along Spuy & Outlet Channel Looking West



USE manning equation

V = (1.49/n) R^{2/2} 5/K: where N = 0.013, 5= 10/350:0.0857

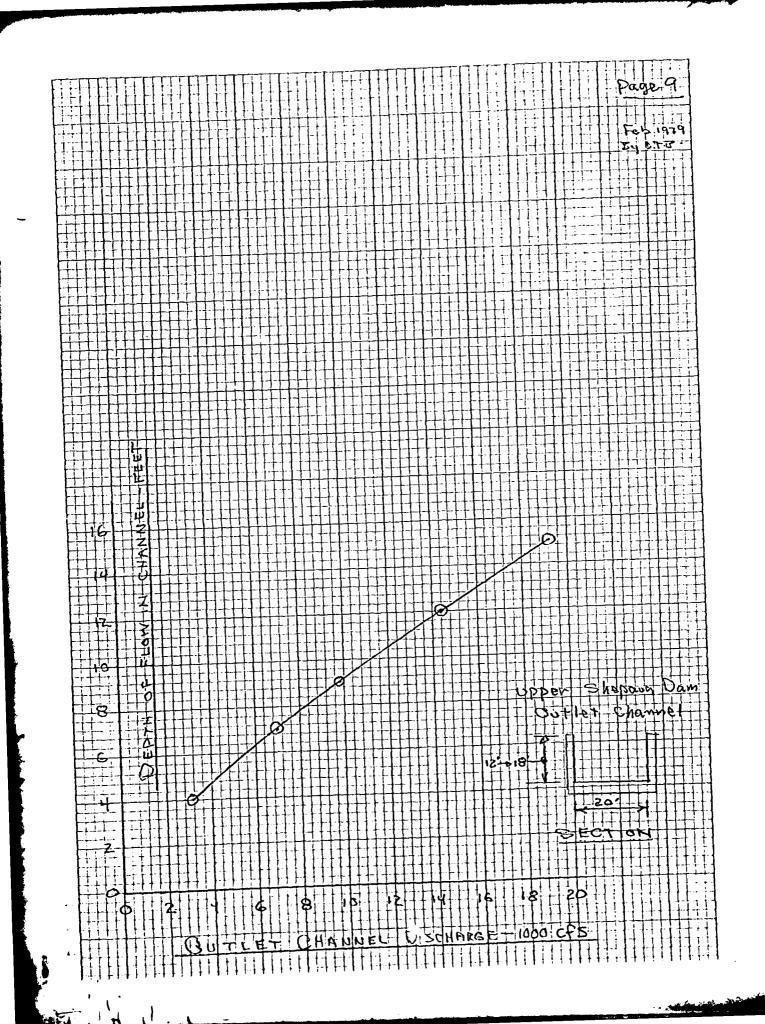
O = AV

S' = 0.1690

.. O = A 1.49 x R^{2/3} 5/K = A R^{2/3} (19.37)

Depth	Area	R	15 8/3	Q 7	
	7.7			cf r	
10	200	. 5	2.92	11,315	545
12	240	5.45	3.10	14,403	graph
14	08 s	5.83	3.24	17,573	next
15	300	6.0	3,30	19,185	bade
,۹	180	4.74	2.82	9,833	l
* 7	140	4.12	2.57	6,966	
* Max	donth	. ha	halina	and the later of the	

* Max dopth in channel before possibility of submerging weir!



Feb. 1979 By DT Belbu

depth aftor

Evaluate pessibility of spillusary becoming submerged - USA Kings Kandbook, 5th edition, page 5-18, figure 5-5, curve #2. While Figss 15 not applicable to broadcrosted weres it will serve as an indication of flow relationships.

<u>_</u>	elev 915.0
2 2 2 2	- Z - HI
9 3	Clev 910.0
2 2 2	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Vertical Sect	my thru spuy Set graph, page 9 for cold

VENTI	cal 5	ection that spi	37 <u>/</u>	C 39 . wa	flows !	from c	01. () E. (C)
		©	Ò	3	9	<u>(3)</u>	(C)	$\widehat{\mathcal{O}}$
Elov	HI	Ą	Ð,	Hz	Hz/H)	Q/Q,	CQ ₅	OTOTAL .
		(tree pischade)	Channel Depth		F19 5-5	iiq 5-5	262 263 263	
₹		(ct2)	(f.f.) (f.f.)	(ċ+)	J. J.		-,-	@*@+@
915	5	4360	5	- 2.	~ .	•		4,360
917	7	7273	7.5	+0.5	73.0	1.0	306	7,529
913	8	8825	8-8	8+1	0.23	0,95	562	8,946
919	9	10,530	16.1	. 3.1	0.34	0.91	884	10,446
920	10	12,333	11.5	4.5	6.45	0.69	1507	11,813
922	12	16,212	14-4	7.4	0.62	87.0	2000	14,645

Comments

- *1. The 2000 cfs was kept separate as the final O of 14645 cfs 15 = to 14,403 cfs as found on page 7 indicating the flow the channel would take with a 12' depth. which would not arentep the channel training walls.
 - 2. The about approach for arriving @ O rord, Column (?) is felt to be rational in the sancy that it takes pertinent factors into account.

Feb 1979 By D.T. Ballow

Comments continued

3. The 7' depth in the channel that was utilized before submargence took place exists @ the upstram end only.

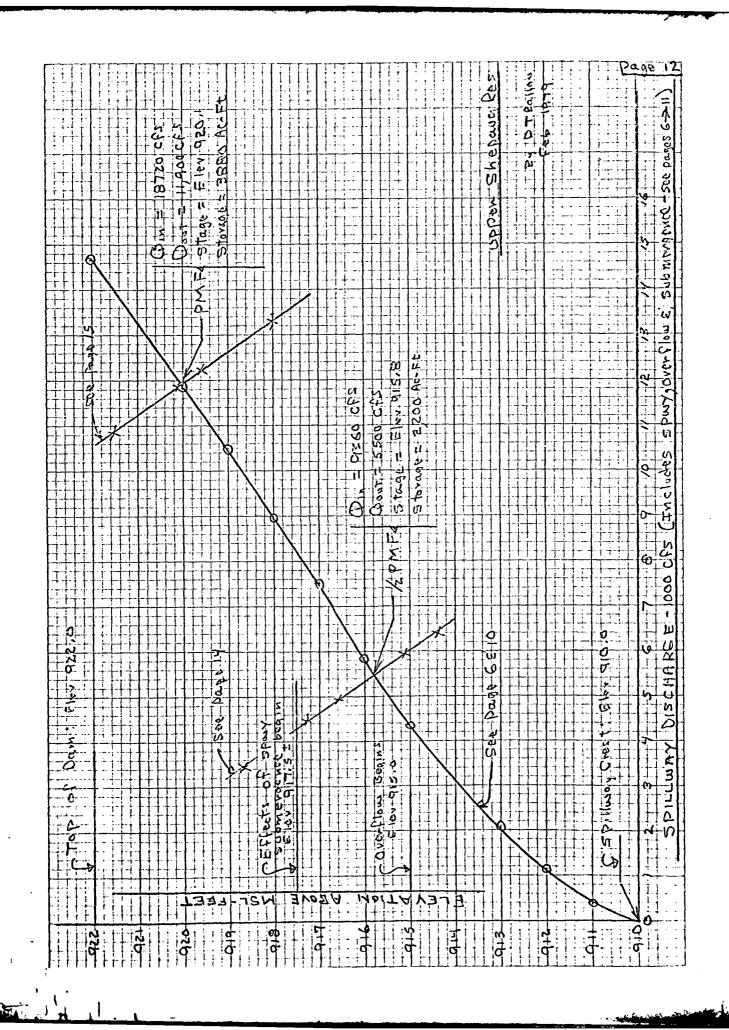
The channel is = 2.8' deeper, due to slope, @ the south end of the spillway.

This method of appraisal will work in a conservative direction as regards outlet works discharge capability. i.e.,

The outlet works will probably pass a greater flow than indicated. It is felt that further refinement would be inappropriate.

At this point we are ready to graph the data of page 10 and commence the shortcut routing procedure to datermine capability of structure to pass a storm equivalent to the KPMF E'. PMF

Data to be utilized from page 10
15 Eter versus column (7). flow
below eter 915.0 may be obtained
from page 6.



Feb 1979 By D.T. Eallou

Routing of KPMF. = 9360 CFS

Check maximum storage by short-cut routing method for & par as the minimum critoria to satisfy the SDF. Then detormine what % of the PMF Is passable without overtopping the structure. (Dam).

PPOR of 1 PMF = 9360 CFS

Select surcharge storage associated with a flow of % PMF. This is a baginning Point atilized in order to select covered lower E, higher points to use in routing.

For Op = 9360 cfs the stage -discharge graph (page 12) indicates elev 918.32

For elev 918:3 the stage-storage work on page 5 reflects 3150 AC-Ft. This would be:

$$\left(\frac{3150 \text{ AC-Ft}}{6656 \text{ Acres}}\right)\left(12 \frac{n}{\text{Ft}}\right) = 5.68 \text{ inches of RO. = Storics}$$

FEB 1979
By B.T Eallou

Ca	ntinue Ro	priture	al /2 PMF	_
•	②	3	(P)	Ś
Stor(i)	$\left(1-\frac{5 \operatorname{Tor}(i)}{9.5}\right)$	stor(c)	Op:	Flev.
inche 5	(15)	Ac-Ft (①×Area)	@^4360	from page 5 for Col 3
6.0	0.368	3,3 28	3444	918.7
5.68	0.402	3,150	3763	6.816
5.0	0.474	2,773	4437	917.3
4.5	0.526	2,496	4923	916.6
3.5	0.632	1941	5916	9,5,1
3.0	0.684	1664	6402	914.4

Note: Columns (D E. B) are platted
on page 12 to indicate
movimum reservain terel E.

Spury discharge for this
routing of 1/2 PMF: = 9360 cfs.

Maximum Reservoit Elev = 915.8 Maximum Discharge = 5,500 Cfs Maximum Starage = 3200 Ac-F2 (Soc page 5)

vote that Top of Dam = else 922.0

Try Routing the PMF E', see where it falls

Routing of PMF. = 18720 cls = Op.

For a beginning point select surcharge storage associated with 60% of PMF, which = 11,232 Cfs

For Q=11, 2:2 cfs the stage - Discharge curve (Page 12) indicates alev 919.6

For the 919.6 the stage-storage curul, (pages) indicates 3,670 AC-Ft.

3670 AC-Ft x 12 1/2 = 6.62 d RO. = Stori)

Ob! = Ob! (1 - \frac{10.0}{240.01} = 18\frac{150}{250} (1 - \frac{10.0}{240.01})

0		(3)	(1)	(5)
stor(i)	$\left(1-\frac{13}{2 + 0.4.!}\right)$	Storic)	Op:	Elev.
inches	(left)	AC-Ft Ox Arca	cf 2	for cel 3
8.00	0.579	4437	10839	921,5
7.00	0.632	3883	11,831	920.1
6.62	0.652	3672	12,205	919.6
5.50	0.711	3051	13,301	018.0

Columns DE! B are plotted on page 12 E' indicate:

- 1. Mar Roservan Lovel = Eku 920.1
- 2. Max Discharge = 11,900 cfs
- 3. May Stevage = 3880 Ac-Ft (50895)

84. P. Bollon BA-01 1,030

Breaching Analysis & Comments

Test Flood Stage = Ebr 920.1

Dam Low Pend = Elev 835.0

A = 85.1

width halfway up = 600° width halfway up = 600°

Φρ, = ξ7.180 × Vg (85.1)²⁵
= 237,572 cf 5

Total Storage to Top of Dam = 14, 700 ACFE

A. downstream vouting was not accomplished as thong is only about 1500 feet of uninhabiled valley that lies between upper Shopang Dam and the upstream reaches of Shepang Reservoir, both important water supply facilities for the waterbury area. The shepang dam was breached and downstream water profile to the town of woods-ville was establish.

Comments

The size E. hazard classification indicated a SDF of the PMF, both KPMF E. the PMF were evaluated and the results may be viewed on page 12.

There appears not to be any problems associated with overtopping. as the KPMF left a freeboard of 6.2 feet and the PMF left a free-board of 1.9 feet.

More of the conduits were utilized in mouting the Test Flood"

may 1979

Kote:

Relative storage capabilities of Uffer Shepang & Shepang.

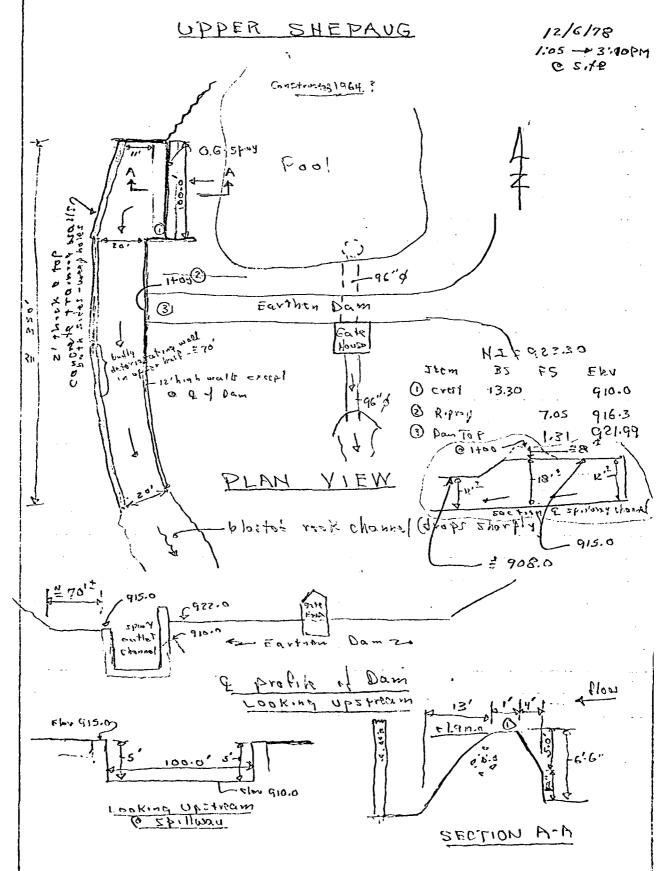
- L Upper Shepava to top of dam has an approximate "total storage = 14,700 Acts.
- 2. Shepard to top of Dam = 3000 Ac-St ... 5puy 0401 = 2000 Ac-St
- 3. With water loved in Shapong @ the spay ovest stex of \$19.0 & Upper Shepang releasing its total storage of 14,700 Ac-Ft the surcharge @ Shepang would be @ elev \$976.0 which = 77 fat (seventy-seven feet) above the Shapang Spay crest. This is based on a volumetric companion andy. (see nort page)

Comments continued

A more realistic approach utilized the breaching of 237 572 cfr (su parch) E' detormine this point on the discharge rating curve or data for Shopang Dam. This was done E' a 33.5. head own the spillway Crest 3 Shepang Dam was found to pass the 237, 572 cfr.

Then for instead of 77' color 896 c Shepany we would attain 32.5' c a box 852.5 = 5 the morkinum of lasting had due to a boxaching of Upper Shepang Dam.

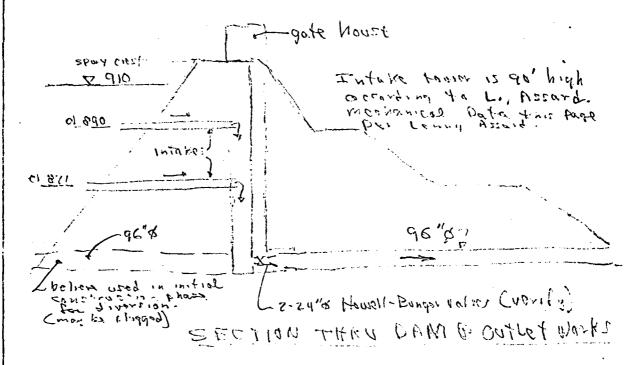
There exists for better delineated methodology on the for-gone discussion under item 3 (this item). However, within the scape of this project it containly is not warranted.

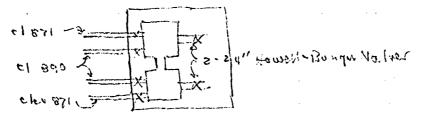


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12/6/78





FLAN VIEW

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	Finding	Reservoir	Level
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	HI=	902.53	
11年7十	5,64		896.39
on 1500 care	ind	13.98	688.35

mayor part = 23.44,

APPENDIX E

INVENTORY OF DAMS

INVENTORY OF DAMS IN THE UNITED STATES

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